

Pre-amp EDFA ASE Noise Characterization for Optical Receiver Transmission Performance Optimization

Akram Abu-aisheh, Hisham Alnajjar
University of Hartford
abuaisheh@hartford.edu, Alnajjar@hartford.edu

Abstract

Amplified Spontaneous Emission (ASE) noise mitigation from a pre-amp Erbium Doped Fiber Amplifier (EDFA) to the Photon Detector (PD) in optical receivers can be reduced by minimizing the EDFA ASE noise at the optical receiver level to achieve optimal optical receiver transmission performance.

The photon detector used in optical receivers is either a PIN diode or an avalanche photo diode (APD). APDs have higher sensitivity than PIN diodes, but they exhibit excess noise that degrades the optical receiver transmission performance. On the other hand, PIN diodes have better noise characteristics than APDs. So, optimal optical receiver transmission performance can be obtained by using a combination of a pre-amp EDFA for good sensitivity and a PIN photon detector for low noise.

Introduction

The basic design of an optical receiver consists of an EDFA, an optical band pass filter, a photon detector, a limiting amplifier, and an electrical low pass filter [1]. Pre-amp EDFAs are becoming an integral part of optical receivers since their performance is interrelated to the performance of the receiver photon detector. The generation of ASE noise in a pre-amp EDFA is an effect of the spontaneous de-excitation of the excited erbium electrons. As the electrons have a finite excited state lifetime, some of the electrons return spontaneously to the ground state emitting a photon that has no coherence characteristics with respect to the incoming optical signal, as opposed to a photon generated by stimulated emission that collection of such spontaneously generated photons, being multiplied by the fiber amplifier, forms background noise. This background noise is known as amplified spontaneous emission, and it is the dominant noise element in pre-amp EDFAs. Measuring ASE and its effect on the deterioration of the signal to noise ration for EDFAs can be measured [3].

Erbium Atomic Structure

Erbium atomic structure has three energy levels that are of interest for the study of its amplification characteristic for communication use. In 3-three level erbium atomic structure, population inversion can be achieved using laser pumping at 980nm to excite electrons to the

upper erbium atomic state. When excited to the upper state, electrons rapidly decay non-radioactively to the meta-stable state. If electrons in the meta-stable state are not stimulated within the electron lifetime in that state, electron transition to the lower states results in spontaneous emission. Spontaneous emission is a random emission that introduces noise. The behavior of the erbium doped fiber atomic structure is described in the following level rate equations [3]:

$$\frac{dN_3}{dt} = -\frac{N_3}{\tau_{32}} + (N_1 - N_3) * \sigma_p * S_p \quad (1)$$

$$\frac{dN_2}{dt} = -\frac{N_2}{\tau_{21}} + \frac{N_3}{\tau_{32}} - (N_2 - N_1) * \sigma_s * S_s \quad (2)$$

$$\frac{dN_1}{dt} = \frac{N_2}{\tau_{21}} - (N_1 - N_3) * \sigma_p * S_p + (N_2 - N_1) * \sigma_s * S_s \quad (3)$$

Where, N is the population density at the given level [1/cm³], S is the photon flux [1/cm² * s], τ is the spontaneous lifetime [s], and σ is the transition cross section [cm²]. The first equation describes the population change rate for the upper state, the second equation describes the population change rate for the meta-stable state, and the third equation describes the population change rate for the ground state. The steady state atomic populations N1 and N2 are functions of the pumping rate which represents the pump absorption rate between levels 1 and 3, and of the absorption and stimulated emission rates between levels 1 and 2. Figure 1 shows the 3-level erbium atomic structure, and it shows the level transitions when erbium is used in a single stage 980 nm pumped pre-amp EDFA [4]. The sum of the population in the three states of the erbium atomic structure is equal to the total population. The sum of the population in the three states is equal to the total population.

$$N = N_1 + N_2 + N_3 \quad (4)$$

Under a steady state condition, electron transition is given by:

$$\frac{dN_1}{dt} = \frac{dN_2}{dt} = \frac{dN_3}{dt} = 0 \quad (5)$$

The basic principle of signal amplification in erbium doped fiber is based on the fact that when an optical signal passes through erbium doped fiber, the signal is amplified due to stimulated transition between electronic states in the presence of electromagnetic radiation at the correct wavelength to achieve population inversion. In order for signal amplification to happen [5], a frequency f_{12} is needed where

$$f_{12} = \frac{E_1 - E_2}{h} \quad (6)$$

Here, h is Plank's constant = 6.626x10E-34 [J/s].

Stimulated photons are in coherence with the input signal, and that results in signal amplification. In free space, the radiation wavelength is given by:

$$\lambda_{21} = hc / (E_2 - E_1) \quad (7)$$

When this radiation interacts with a photon in the lower energy level, the photon is transformed into the upper atomic level. If a photon in the excited state is not stimulated within the 10 ms lifetime of the excited state, it will spontaneously decay to the ground state producing ASE. When this photon travels through the erbium-doped fiber, it gets amplified resulting in amplified spontaneous emission. All the excited ions can spontaneously relax from the upper state to the ground state by emitting a photon that is unrelated to the signal photons. This spontaneously emitted photon can be amplified as it travels down the fiber and stimulates the emission of more photons from excited electrons.

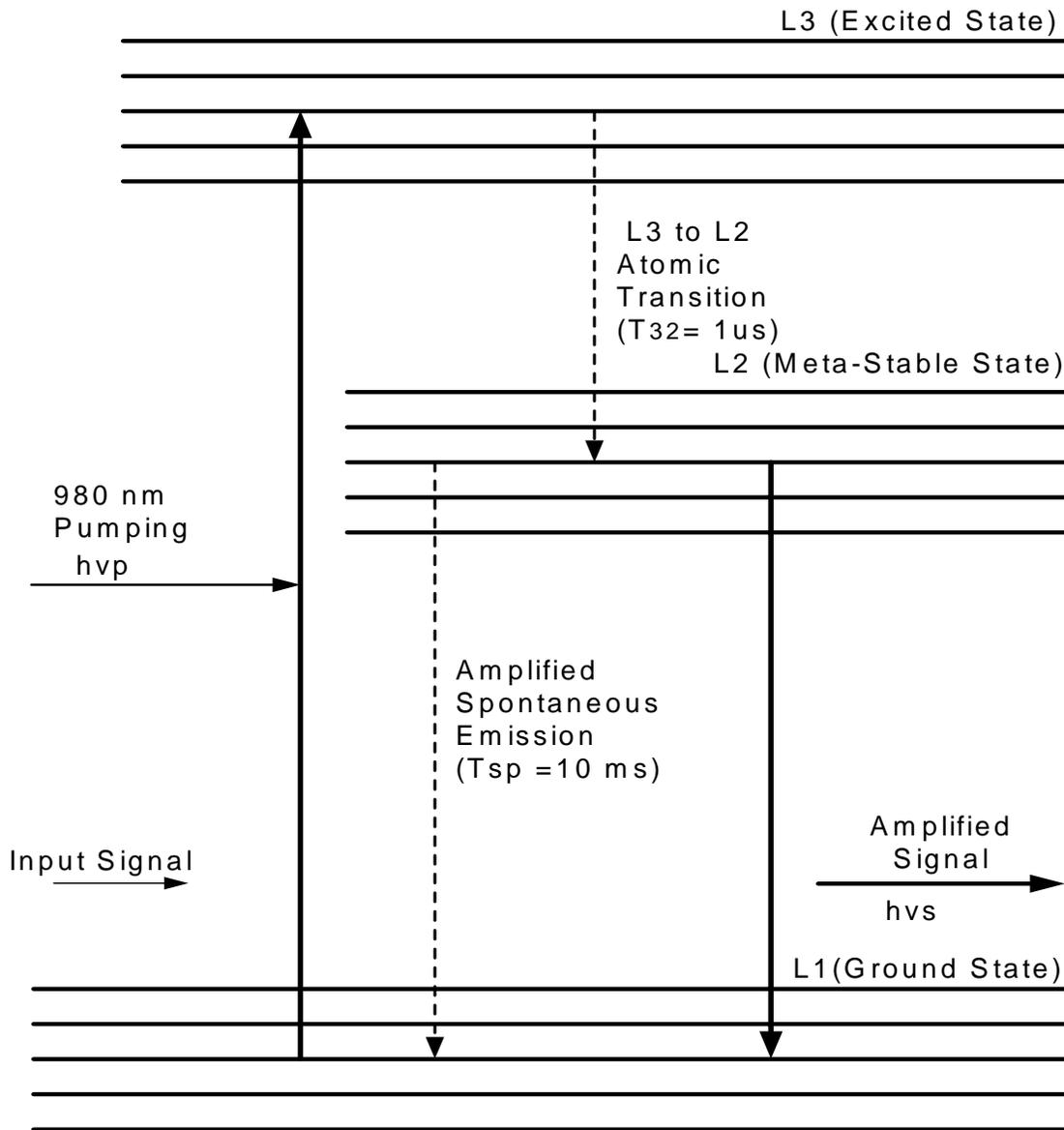


Figure1: 980 nm pumping in Erbium atomic structure

Amplified spontaneous emission can occur at any frequency within the fluorescence spectrum of the amplifier transitions. The dominant noise source in any EDFA is amplified spontaneous emission. This spontaneous emission reduces the amplifier gain by consuming the photons that would otherwise be used for stimulated emission of the input signal. In single mode fiber, the noise output power resulting from amplified spontaneous emission is given by [6]:

$$P_{ASE} = 2 * n_{sp} (G - 1) h\nu \Delta(\nu) \quad (8)$$

The total amplified spontaneous emission at any point in the fiber is the sum of all amplified spontaneous emission power from the previous sections in the fiber and the amplified spontaneous emission at the given fiber point. In order to minimize ASE noise, the pump power should be just enough to achieve population inversion. Population inversion can be achieved when the population in the excited state, N_2 , is greater than the population in the ground state N_1 . The threshold pump power required to achieve population inversion can be obtained by setting the rate equation of level 2 to 0, and setting N_1 to be equal to N_2 . A long meta-stable state lifetime and a large absorption cross section are needed to have a low pump threshold to achieve population inversion. A detailed analysis of EDFA and photodiodes noise elements was performed by different researchers [7] & [8].

Optical Receiver Transmission Performance

Optical receiver transmission performance, commonly known as bit error rate (BER) performance, is the gauge by which optical receivers are characterized. It characterizes the ability of the receiver to perform up to the transmission performance specifications under the same test conditions as those where the receiver operates in the field [4]. So transmission performance will be used to analyze the optical receiver performance under different operating conditions. Since the most important factor in the pre-amp performance is how well it performs in the optical receiver, the optical receiver optimal transmission performance analysis under different operating conditions is the ultimate method for characterizing pre-amp EDFA noise performance. The pre-amp EDFA design needs to be optimized at the pre-amp level and the EDFA level. Then the pre-amp performance should be determined by how well the pre-amp performs in the optical receiver.

For optimal optical receiver transmission performance, the pre-amp EDFA design must be coordinated with the photon detector design in order to minimize amplified spontaneous emission noise mitigation from the pre-amp EDFA to the photon detector and the photon detector signal-spontaneous beat noise. The pre-amp input power, output power, and operating wavelength should be taken into account. This allows designers to choose the right erbium doped fiber length and pump power combination, and it helps minimize amplified spontaneous emission at the output of the pre-amp EDFA.

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optical receiver, optical receiver optimal transmission performance analysis under different operating conditions is the ultimate method for optimizing pre-amp EDFA performance in the optical receiver. The pre-amp EDFA design needs to be optimized at two levels: the pre-amp/photon detector subsystem level and the optical receiver level. Several characterization experiments were performed to analyze the effects of changing the pre-amp operating conditions on the optical receiver transmission performance. Testing the pre-amp-based optical receiver at a fixed signal-to-noise ratio at 1550 nm, the transmission performance was recorded at different input/output combinations. A graphical representation of the optical system transmission performance results, after normalizing BER, is given in Fig. 2 [1].

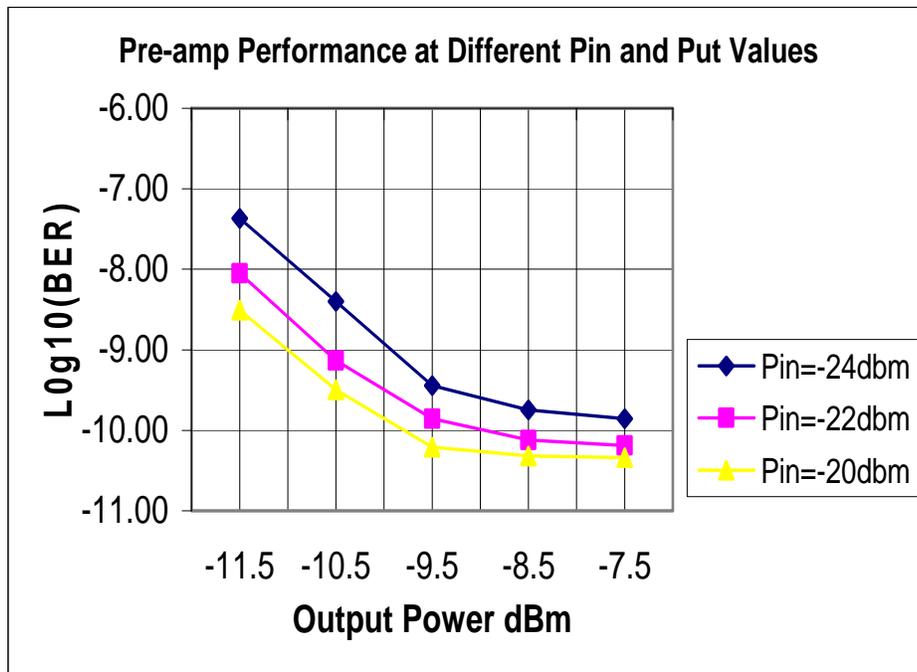


Figure 2: Optical receiver performance change at different input and output power levels

From the results in figure 3, we see that the optical receiver transmission performance improves as the pre-amp output power is increased. This improvement is due to the fact that more output power requires more pump output, and more output power excites more electrons to the upper state. This excitation will result in the population inversion that is needed for the amplification process.

Testing the pre-amp-based optical receiver at different input powers and at different signal to noise ratios at fixed output power and input signal wavelength, the transmission performance changes due to the changes in the operating conditions were monitored, and the results are given in figure 3 [1]. A graphical representation of the system transmission performance, after normalizing is given in figure 3 that shows that the optical receiver transmission performance improves as the pre-amp input signal power is increased.

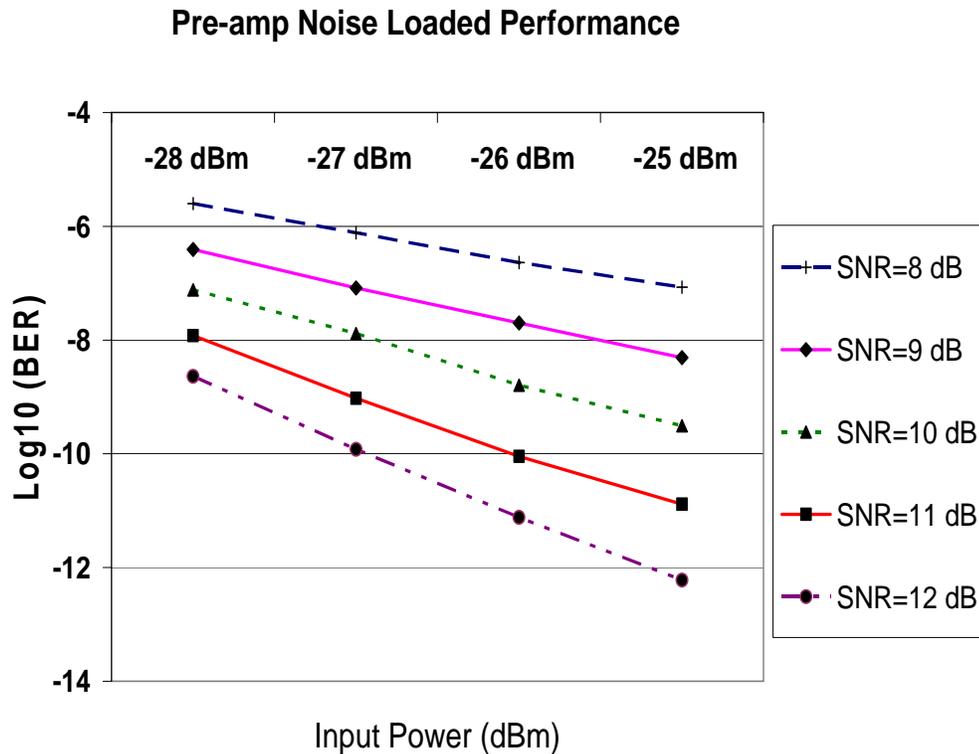


Figure 3: Optical receiver performance at different input powers and different input signal to noise ratios

At the atomic structure level, an increase in the input power causes more stimulated emission of the excited electrons. This leaves fewer electrons to move to the ground state spontaneously. This means that the pre-amp is generating less amplified spontaneous emission, and this reduces the signal spontaneous noise in the photon detector which results in improved optical receiver transmission performance

Conclusion

Since the most important performance factor in the pre-amp performance is how well it performs in the optical receiver, the optical receiver optimal transmission performance analysis under different operating conditions is the ultimate method for characterizing pre-amp EDFAs noise performance. The results of the tests performed for this work shows a need for designing the pre-amp EDFA and photon detector as one subsystem. Then the pre-amp EDFA needs to be fine-tuned at the optical receiver level to achieve optimal optical receiver transmission performance. For optimal optical receiver transmission performance, the pre-amp EDFA design must be coordinated with the photon detector design in order to minimize amplified spontaneous emission noise mitigation from the pre-amp EDFA to the photon detector. This will minimize the photon detector signal-spontaneous beat noise.

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Biography

AKRAM ABU-AISHEH is an Assistant Professor in the Electrical and Computer Engineering Department in the College of Engineering, Technology, and Architecture at the University of Hartford. He has a Ph.D. in Optical Communications from the Florida Institute of Technology and MS. and B.S. degrees in Electrical Engineering from the University of Florida. He has seven years work experience as a Senior Fiber optic communications Test Process Engineer at Tyco Telecommunications, and his main research interests are in the areas of Power Electronics and fiber optic communications. Professor Abu-aisheh is also the program director of the electronic and computer engineering technology program in the college of Engineering, Technology, and Architecture at the University of Hartford.

HISHAM ALNAJJAR is an Associate Professor of Electrical and Computer Engineering at the University of Hartford, Connecticut (USA), where he is also the Associate Dean of the College of Engineering, Technology, and Architecture (CETA). Before that he served for nine years as the Chair of the Electrical & Computer Engineering Department at the University of Hartford. Ph.D. from Vanderbilt University, M.S. from Ohio University. His research interests include sensor array processing, digital signal processing, power systems in addition to engineering education.